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# High-speed visible light communication based on micro-LED: A technology with wide applications in next generation communication

Tingwei Lu<sup>1</sup>, Xiangshu Lin<sup>1</sup>, Wenan Guo<sup>1</sup>, Chang-Ching Tu<sup>3,4</sup>,  
Shibiao Liu<sup>1</sup>, Chun-Jung Lin<sup>5</sup>, Zhong Chen<sup>1,2</sup>, Hao-Chung Kuo<sup>3,4\*</sup> and  
Tingzhu Wu<sup>1,2\*</sup>

The evolution of next-generation cellular networks is aimed at creating faster, more reliable solutions. Both the next-generation 6G network and the metaverse require high transmission speeds. Visible light communication (VLC) is deemed an important ancillary technology to wireless communication. It has shown potential for a wide range of applications in next-generation communication. Micro light-emitting diodes ( $\mu$ LEDs) are ideal light sources for high-speed VLC, owing to their high modulation bandwidths. In this review, an overview of  $\mu$ LEDs for VLC is presented. Methods to improve the modulation bandwidth are discussed in terms of epitaxy optimization, crystal orientation, and active region structure. Moreover, electroluminescent white LEDs, photoluminescent white LEDs based on phosphor or quantum-dot color conversion, and  $\mu$ LED-based detectors for VLC are introduced. Finally, the latest high-speed VLC applications and the application prospects of VLC in 6G are introduced, including underwater VLC and artificial intelligence-based VLC systems.

**Keywords:** visible light communication;  $\mu$ LEDs; modulation bandwidth; detector; 6G

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## Introduction

Innovations in smartphones and smart homes, and the emergence of online services have propelled the growth of cloud computing, the Internet of Things, and autonomous driving<sup>1-6</sup>. In the future, the metaverse, a fledgling networking technology, will allow users to experience multimedia by combining distributed real-time sources and stored digital assets in real time. However,

its real-time interactive nature will significantly increase requirements for data storage and transmission rates<sup>7,8</sup>. With the increasing demand for data traffic by users, licenses for spectrum resources will become expensive and scarce<sup>9</sup>. It is unlikely that a single communication technology will be able to support these growing data demands. Therefore, future networks must support the coexistence and cooperation of different wireless

<sup>1</sup>School of Electronic Science and Engineering, Fujian Engineering Research Center for Solid-State Lighting, Xiamen University, Xiamen 361005, China; <sup>2</sup>Innovation Laboratory for Sciences and Technologies of Energy Materials of Fujian Province (IKKEM), Xiamen 361005, China; <sup>3</sup>Department of Photonics and Graduate Institute of Electro-Optical Engineering, College of Electrical and Computer Engineering, Yang Ming Chiao Tung University, Hsinchu 30010, Taiwan, China; <sup>4</sup>Semiconductor Research Center, Hon Hai Research Institute, Taipei 11492, Taiwan, China; <sup>5</sup>Guangdong Visible Light Communication Technology Co., LTD., Foshan 528000, China.

\*Correspondence: HC Kuo, E-mail: [hckuo@faculty.nctu.edu.tw](mailto:hckuo@faculty.nctu.edu.tw); TZ Wu, E-mail: [wutingzhu@xmu.edu.cn](mailto:wutingzhu@xmu.edu.cn)

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technologies, including radio-frequency (RF), millimeter-wave, and light-wave technologies<sup>10,11</sup>.

Light-emitting diode (LED) solid-state lighting technology offers low power consumption and cost, small size, and a long operational lifetime; moreover, it is environmentally friendly. These advantages contributed to the explosive growth of the LED-lighting market<sup>12–18</sup>. Notably, the visible-light band with a spectral range between 380 and 780 nm is not licensed like radio frequencies and can be used without authorization<sup>19–23</sup>. Hence, LED-based visible light communication (VLC) technology has attracted research attention worldwide, and VLC technology has rapidly developed in the past decade<sup>15,24–26</sup>.

The flickering of LEDs cannot be identified by the naked eye, owing to the high frequency of the signal in the VLC system. Thus, by adding relatively inexpensive front-end components, VLC can be easily implemented in existing lighting infrastructures to achieve data communications with speeds in the Gbps range<sup>27–31</sup>. Furthermore, compared with the considerable co-channel interference of wireless RF communication, the propagation of visible light is not perturbed by electromagnetic waves, i.e., the electromagnetic interference phenomenon does not occur<sup>32</sup>. Therefore, VLC offers unique advantages in hospitals, airports, nuclear power plants, underground mines, substations, and other scenarios that are sensitive to electromagnetic interference. Accordingly, the advantages of VLC technology, such as environmental protection, stability, and confidentiality in the transmission process, make it a candidate for broad application prospects<sup>33–35</sup>.

A unique advantage of VLC is that it can simultaneously realize illumination and displays. Owing to their high efficiency and environmental protection, white light emitting diodes (WLEDs) are considered an efficient and energy-saving solid-state light source and have received considerable attention<sup>36–39</sup>. Traditional WLEDs consist of blue and violet LED chips and phosphors. Despite the excellent performance of phosphor-based WLEDs, their modulation bandwidth is significantly limited by the color-conversion materials<sup>40</sup>. To accurately transmit high-speed data, the switching time between turning the LED on and off should be as short as possible. Thus, the device should have a short fluorescence lifetime. Therefore, the exploration of luminescent materials that can be mass-produced with high efficiency and response speed is of great significance for next-generation WLED

applications.

Although LEDs have attracted considerable interest in high-speed VLC applications, many factors limit the modulation bandwidth of conventional LEDs<sup>41,42</sup>. Recently, research has gradually focused on the application of micro-LEDs ( $\mu$ LEDs) with an active area of less than 100  $\mu\text{m}$  in VLC. Compared with conventional LEDs,  $\mu$ LEDs have a higher modulation bandwidth owing to their smaller size, higher injection-current density, and lower RC time constant, which significantly improves the transfer rate of VLC systems<sup>43–46</sup>. Moreover,  $\mu$ LEDs can be employed in displays; thus, they can be used for combined full-color display and communication applications. The compactness of  $\mu$ LEDs makes them easier to integrate; therefore,  $\mu$ LED-based VLC systems also endow wearable devices with unique advantages<sup>47,48</sup>. In addition, their sensitivity to light has enabled the use of  $\mu$ LEDs in the fabrication of high-performance receivers, which provides new possibilities for their application<sup>49</sup>.

With the continuous advancement of 5G commercialization, future-oriented competitiveness research has begun in the field of its successor 6G<sup>50</sup>. The 6G white papers released by several research institutes show that 6G communication is no longer limited to the original wireless spectrum<sup>51</sup>. New spectrum resources can be found in the visible-light band. As one of the two major future spectrum resources, VLC can exploit the ultrahigh bandwidth in the 400–800 THz frequency range. Compared with traditional wireless frequency bands, the unlicensed spectrum used by VLC will give operators and device manufacturers more freedom, thereby establishing a technology that is suitable for 6G<sup>52</sup>. In the indoor environment, VLC has the inherent advantages of wide coverage, green light, and energy saving. In the outdoor environment, VLC technology can be used in underwater communication, inter-vehicular communication, and several other unique applications for realizing machine-machine interaction<sup>53,54</sup>. Owing to the high requirements for 6G in terms of transmission speed, VLC based on high-bandwidth  $\mu$ LED devices and artificial intelligence (AI) will emerge in various application fields of 6G<sup>55</sup>. Although  $\mu$ LEDs are now widely used in VLC, few studies have provided general descriptions of  $\mu$ LED-based VLC systems from devices to applications. An extensive review of high-speed  $\mu$ LED-based VLC will facilitate its comprehensive application to future 6G.

In this review, we focus on the  $\mu$ LED-based high-speed VLC system and its applications, as illustrated in

Fig. 1. First, the advantages and challenges of using  $\mu$ LEDs in VLC systems are summarized. Methods to improve the modulation bandwidth of  $\mu$ LEDs are comprehensively discussed, including c-polar epitaxial structure optimization, semi/nonpolar GaN epitaxial growth, microstructures, and InGaN quantum dots (QDs) as active regions. Furthermore, photoluminescent and electroluminescent WLEDs for VLC are introduced and discussed separately according to different fabrication methods. Progress in the use of  $\mu$ LEDs for VLC detectors is also discussed. Finally, the latest high-speed VLC applications and the application prospects of VLC in 6G are discussed.

### Overview of micro light emitting diode ( $\mu$ LED)-based visible light communication (VLC) systems

#### Theory of VLC applications

The transmitter in a VLC system uses a visible-light-emitting device, such as an LED or LD, to realize data transmission<sup>56,57</sup>. LEDs with diffusers, energy-saving properties, and environmental protection are good light sources for providing uniform illumination. The receiver

consists of a photodetector (PD) and signal-processing circuitry. After receiving the optical signal and restoring it to a current signal, the PD generates a voltage signal and completes the digital-to-analog conversion after the signal passes through the signal-processing circuit. The electrical signal is then amplified, equalized, and demodulated to extract valid data.

The channel characteristics in the VLC are distinct from those of the traditional RF system, which is mainly affected by the light source, free-space atmospheric channel, and PD at the receiving end. The modulation bandwidths of the transmitting and receiving ends jointly affect the overall performance of the VLC system. However, in most VLC systems, where the space channel is relatively stable, the devices at the transmitting end mainly affect the communication performance because of the relatively high receiving bandwidth of the PD.

Frequency response is one of the most important parameters required to address when developing LEDs for VLC-system transmitters. For a LED system, the light transfer function is expressed as follows:

$$H(\omega) = \frac{N_{out}(t)}{N_{in}(t)} = \frac{1}{1 + i\omega\tau}, \quad (1)$$

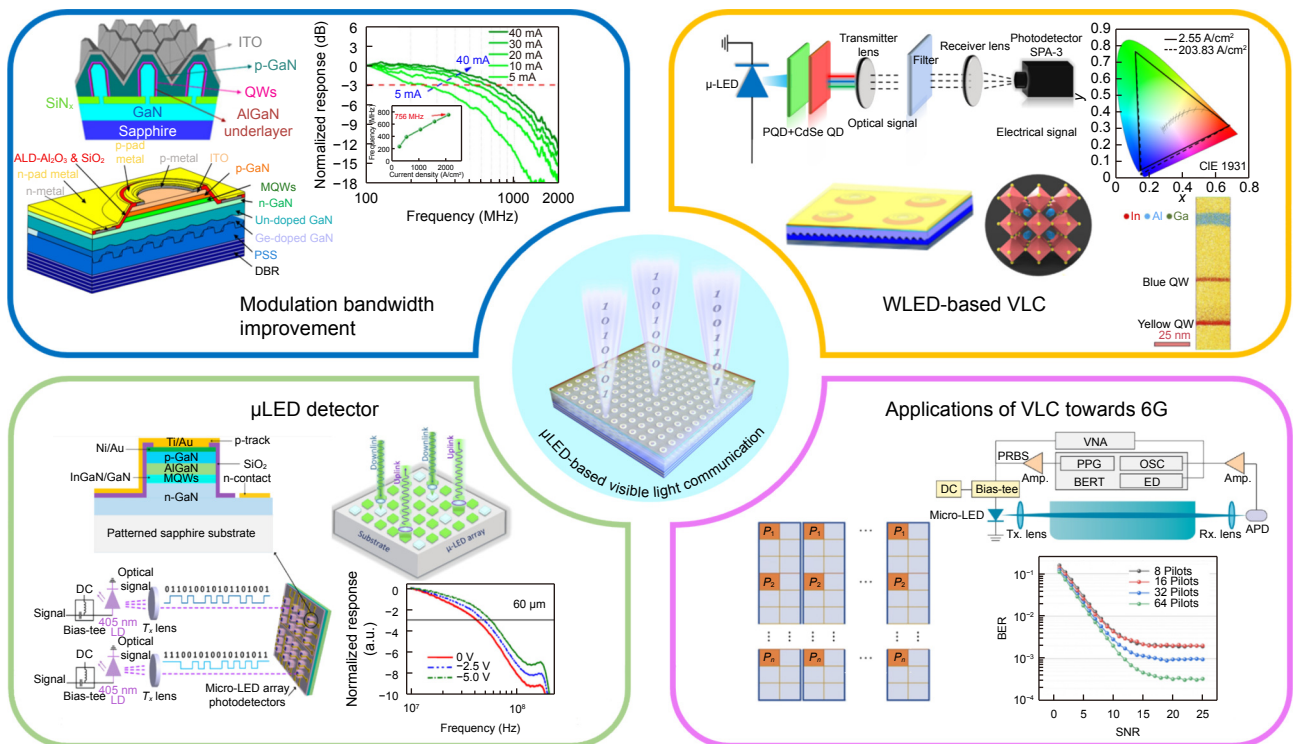


Fig. 1 | Summary of the review, which includes modulation bandwidth improvement, white light emitting diodes (WLED)-based visible light communication (VLC), micro light emitting diode ( $\mu$ LED) detector and applications of VLC towards 6G. Figure reproduced from: ref.<sup>96,125,154,165</sup>, American Chemical Society; ref.<sup>139,153</sup>, Chinese Laser Press; ref.<sup>161,166</sup>, OSA Open Access Publishing Agreement; ref.<sup>175,184</sup>, Optical Society of America.

where  $N_{in}$  and  $N_{out}$  are the input and output carrier concentrations, respectively.  $N_{out}$  determines the modulated optical power.  $\omega$  is the angular frequency, and  $\tau$  is the total response time. The frequency at which the optical modulation power is reduced by half is defined as  $f_c$ ,

$$H(2\pi f_c) = \frac{1}{2}, \quad (2)$$

$$f_c = \frac{\sqrt{3}}{2\pi\tau} = \frac{\sqrt{3}}{2\pi} \left( \frac{1}{\tau_r} + \frac{1}{\tau_{nr}} + \frac{1}{\tau_{RC}} \right), \quad (3)$$

where  $\tau_r$  and  $\tau_{nr}$  refer to the radiative and nonradiative recombination lifetimes, respectively.  $\tau_{RC}$  is the resistor-capacitor (RC) time constant. As observed in Eq. (3), the factors affecting the LED modulation characteristics primarily depend on the RC time and carrier radiation lifetime. The junction capacitance affects the RC time and response speed of LED devices, which can delay the signals. The spontaneous emission lifetime of carriers directly affects the time required for carriers from recombination to photons to escape from the device.

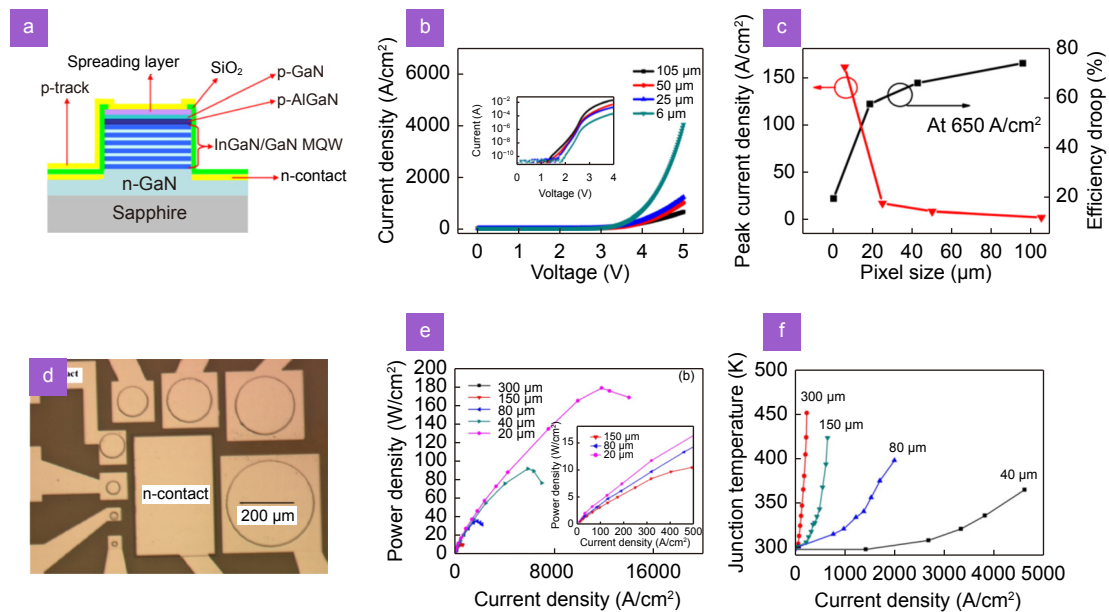
### Advantages of $\mu$ LEDs as VLC transmitters

Commercial large-size GaN-based LED dies have an area of a few millimeters per side. However, over such a large area, the response speed is ultimately limited by its RC time constant<sup>58</sup>. In addition, the carrier recombination process in GaN-based LEDs is affected by the carrier localization effect and quantum confinement stark effect

(QCSE), which also leads to an increased carrier lifetime and reduced electro-optical conversion response speed<sup>59,60</sup>.

A smaller active area results in reduced geometric capacitance, and consequently a lower RC time constant, which allows  $\mu$ LEDs to have higher modulation bandwidths. Furthermore,  $\mu$ LEDs can withstand higher injection current densities, owing to their uniform current spreading. Tian et al. studied the optoelectronic properties of  $\mu$ LEDs of different sizes, as depicted in Fig. 2(a)<sup>61</sup>. The current density–voltage (J–V) curves of the LEDs are illustrated in Fig. 2(b). The results indicated that samples of different sizes exhibited strong size-dependent behavior. The smaller  $\mu$ LED has a more uniform current distribution, which leads to a higher injection current density<sup>62,63</sup>. They also demonstrated that the current crowding of large-scale samples affects efficiency, especially at high injection densities. The external quantum efficiency (EQE) of the samples was measured. As shown in Fig. 2(c), the smaller  $\mu$ LEDs had lower efficiencies at low current densities, and higher at high current densities. Owing to poor current uniformity, large-sized samples cause a severe efficiency decrease at higher injected carrier concentrations, which results in strong Auger recombination at the edges and other nonradiative recombinations. A higher injection current or efficiency significantly improves the performance of LEDs as VLC emitters.

Zheng et al. investigated the impact of device size



**Fig. 2 |** (a) Schematic of the samples' structure. (b) J–V characteristics of samples. (c) Current densities of peak EQE, and the efficiency drop of samples. (d) Optical micrograph. (e) Power density and (f) junction temperature of the samples at different current densities. Figure reproduced with permission from: (a–c) ref.<sup>61</sup>, AIP Publishing; (d–f) ref.<sup>64</sup>, AIP Publishing.

scaling on the light output and self-heating of InGaN LEDs<sup>64</sup>. Figure 2(d) illustrates the optical micrograph of samples with different sizes. The power density versus current density was measured for InGaN LEDs with diameters ranging from 20 to 300  $\mu\text{m}$  (Fig. 2(e)). The study also observed that small-sized samples could withstand higher current densities. The measured junction temperature highlighted in Fig. 2(f) demonstrated that the junction temperature of the smaller samples increased more gradually with the injection current density. They specified 40  $\mu\text{m}$  and 150  $\mu\text{m}$  LED devices for simulation, and the current crowding effect was considered. They discovered significant overheating of the edge of the 150  $\mu\text{m}$  pixel. Thus, the size-dependence effect of the junction temperature can be attributed to the more severe current crowding effect in larger pixels. This explains why smaller samples can withstand higher current densities.

In conclusion, owing to low capacitance and self-heating effect, and good current dispersion,  $\mu\text{LEDs}$  possess smaller RC constants and higher injection current densities than conventional wide-area LEDs, resulting in shorter carrier lifetimes and higher modulation bandwidths. Owing to the ultrasmall area, the output optical power can be increased for long-distance and high-speed communication by assembling multiple  $\mu\text{LEDs}$  into an array.

## Challenges of $\mu\text{LEDs}$ as VLC transmitters

### QCSE

Although  $\mu\text{LEDs}$  can effectively increase bandwidth compared with traditional LEDs, they still face some challenges in VLC applications. First, commercial  $\mu\text{LEDs}$  are typically grown on the (0001) polar *c*-plane sapphire substrates. This leads to a strong QCSE, which results in reduced efficiency at high injection current densities<sup>65</sup>. The current GaN-based epitaxy has a hexagonal crystal structure with the highest symmetry compatibility, which results in spontaneous polarization<sup>66</sup>. Simultaneously, the lattice mismatch between  $\text{In}_x\text{Ga}_{1-x}\text{N}$  and GaN induces strain, which leads to piezoelectric polarization<sup>67,68</sup>. The internal spontaneous polarization and piezoelectric polarization tilt the energy-band, and reduce the radiative recombination rate of the carriers, which results in lower modulation bandwidths. In addition to the modulation properties, the QCSE also leads to a wavelength shift and efficiency decrease as the injection

current density increases<sup>69,70</sup>.

To suppress the QCSE, research has focused on optimizing the epitaxial structure of the device. For example, a thin quantum barrier (QB) can make the carrier distribution more uniform throughout the active region<sup>71,72</sup>. Therefore, a thin QB can enhance radiative recombination in the active region and suppress the QCSE with higher bandwidths than those of thick QB. Furthermore, the effect can also be suppressed by growing devices on semipolar or nonpolar substrates.

### Carrier localization effect

At low current densities, the QCSE dominates carrier recombination and reduces the radiative recombination rate, which is the main limiting factor for the modulation bandwidth. At high injection condition, the Coulomb shielding effect reduces the polarization caused by the QCSE<sup>73,74</sup>. In this case, the carrier localization effect can significantly influence the carrier recombination processes.

The carrier localization effect prevents the nonradiative recombination of carriers inside the quantum well (QW), thereby increasing carrier lifetime<sup>59,75</sup>. Hence, for a device with a strong positioning effect, its modulation bandwidth is reduced accordingly. It has been shown that the thickness of the QW affects carrier localization. Zhu et al. fabricated  $\mu\text{LEDs}$  with different QW thicknesses and evaluated the extent of carrier localization<sup>76</sup>. For MQWs with fewer in components, the carrier localization effect was mainly caused by well-width fluctuations<sup>77</sup>. This suggests that the localization energy can also be evaluated using the variation of the QW band gap. Thus, thicker QW devices with lower MQW bandgap reductions have weaker carrier localization effects, and thus reduced carrier lifetimes.

### Size-dependent effect

The reduced size reduces junction temperature and improves current density distribution<sup>64,78,79</sup>. However, as the chip size decreases to the micrometer level, the proportion of the sidewall area increases. The Shockley–Read–Hall (SRH) recombination caused by the sidewall defects in the active region affects the efficiency of the device<sup>80</sup>. Standard photolithographic techniques introduce severe defects on the surface during dry etching and subsequent processes, which are difficult to avoid during fabrication<sup>61</sup>. As the chip size decreases, the proportion of the sidewall area increases significantly,

and the effect of sidewall defects increases<sup>81,82</sup>. More carriers are trapped by sidewall defects during migration, which reduces the efficiency of radiative recombination<sup>83</sup>. In addition, the SRH recombination is weakened at high injection current densities, which leads to peak EQEs appearing at larger current densities<sup>84</sup>.

To mitigate the performance degradation, researchers focused on eliminating the sidewall defects of  $\mu$ LED that cause nonradiative recombination. Passivation of sidewalls has been demonstrated as an effective method to reduce the effects of sidewall defects<sup>83</sup>. In addition, the sidewall defects caused by dry etching can be partially recovered by thermal annealing at high temperatures<sup>61</sup>.

In addition, as the manufacturing technology of  $\mu$ LED matures, interest in  $\mu$ LED devices with sizes between 1 and 10  $\mu\text{m}$  is increasing. Smith et al. compared the size-dependent EQE of blue and green InGaN  $\mu$ LEDs with sizes as low as 1  $\mu\text{m}$ <sup>85</sup>. The results show that the EQE of blue  $\mu$ LED evidently decreases for smaller devices. Conversely, green wavelength devices exhibit a smaller size dependence, which is attributed to decreasing surface recombination velocities with increasing In content. Consequently, green  $\mu$ LED sizes smaller than 10  $\mu\text{m}$  have higher EQE than blue devices.

### Approaches to increasing the modulation bandwidth

$\mu$ LED, as an emerging VLC emitter, has rapidly developed in recent years and has made impressive achievements. Table 1 lists the academic results of VLC systems based on  $\mu$ LED as a light source in recent years, which helped us gain a comprehensive understanding of the recent progress.

Currently, blue devices are the most mature among visible LEDs. Thus, blue  $\mu$ LEDs exhibit the highest reported modulation bandwidth among all wavelength devices. Currently, c-plane  $\mu$ LEDs have a lower bandwidth than nonpolar or semipolar  $\mu$ LEDs; however, bandwidths greater than 1 GHz can be achieved by structural optimization or growth of microstructures<sup>86,90,95,96</sup>. In addition, the use of QDs as active regions also helps reduce the carrier lifetime of the device<sup>91,93</sup>. The rest of this chapter describes the methods to increase the modulation bandwidth of the  $\mu$ LED device.

### Optimization of C-plane epitaxial structure

InGaN/GaN MQW active regions based on c-plane growth are currently the most mature manufacturing process in the LED industry. Parameter tuning and optimization based on this structure are of great value for the future commercialization of  $\mu$ LED<sup>97</sup>.

In recent years, structural optimization of c-plane  $\mu$ LED devices has been reported, and the improvement of the modulation bandwidth has mainly focused on enhancing the carrier recombination process. Ferreira et al. fabricated GaN-based  $\mu$ LEDs using Pd as the p-contact metal. Metal contacts with low contact resistances were formed by thermal annealing<sup>98</sup>. This helped maintain a higher current density. In addition, the face layer was etched on a sapphire substrate, which limited the matching of n-GaN to the active region, thus reducing the capacitance of the device. Rajabi et al. grew blue LEDs with ultrathin InGaN QWs (1 nm) and GaN barriers (3 nm)<sup>70</sup>. The ultrathin QW device was grown by metalorganic chemical vapor deposition (MOCVD) on a c-plane sapphire substrate. The epitaxial structure included a

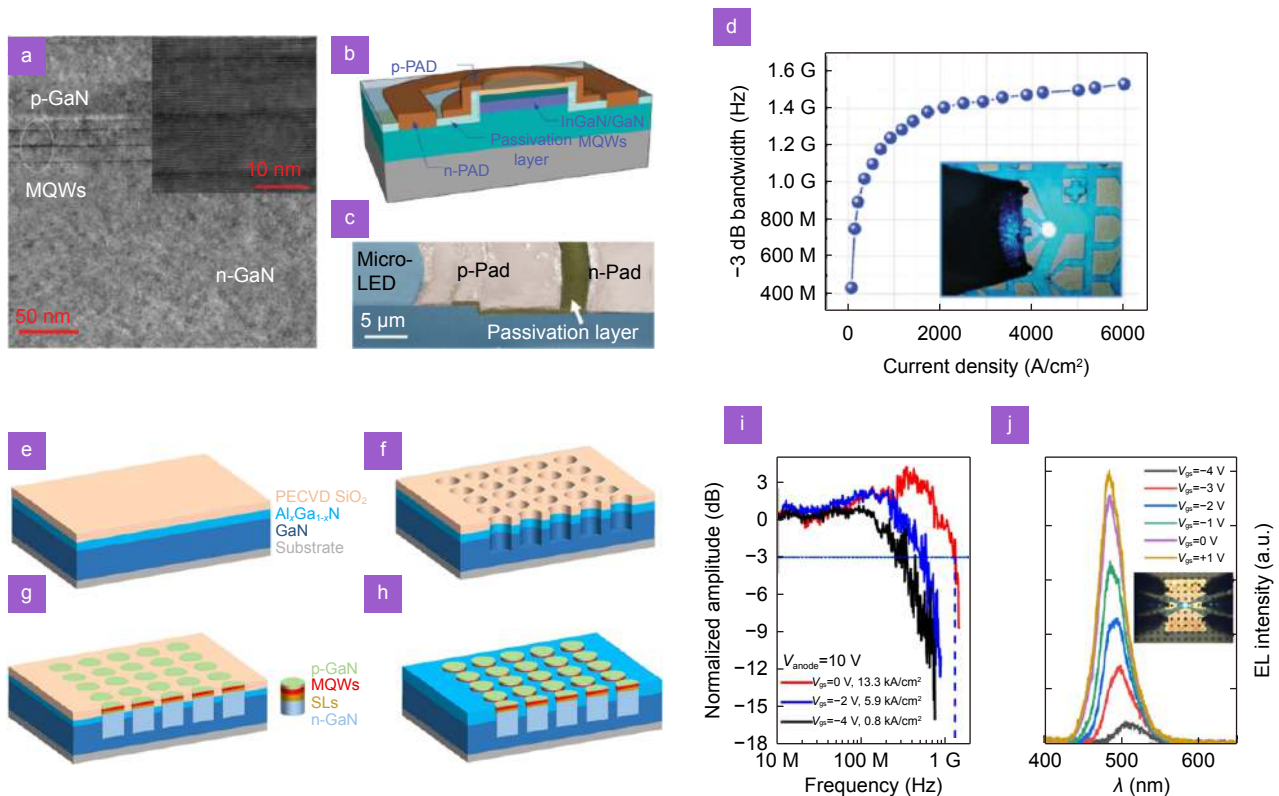
**Table 1 | Summary of research progress in the VLC system based on  $\mu$ LED**

Year	Light source	Modulation bandwidth	Transmission rate	Ref.
2022	c-plane green $\mu$ LED (525 nm)	1.31 GHz	6 Gbps	ref. <sup>86</sup>
2022	Semipolar blue $\mu$ LED (447 nm), yellow phosphor	849 MHz	2.8 Gbps	ref. <sup>87</sup>
2022	c-plane blue $\mu$ LED (450 nm)	880 MHz	1.1 Gbps	ref. <sup>88</sup>
2022	c-plane red $\mu$ LED (652 nm)	271 MHz	350 Mbps	ref. <sup>31</sup>
2022	Nonpolar blue $\mu$ LED (463 nm)	991 MHz	2 Gbps	ref. <sup>89</sup>
2022	c-plane blue $\mu$ LED (475 nm)	1.53 GHz	5.27 Gbps	ref. <sup>90</sup>
2022	Green quantum dot (QD) LED (495 nm)	1.22 GHz	2.1 Gbps	ref. <sup>91</sup>
2021	Semipolar green $\mu$ LED (550 nm)	1.1 GHz	4.3 Gbps	ref. <sup>92</sup>
2021	Green QD-LED (550 nm)	1.3 GHz	none	ref. <sup>93</sup>
2021	c-plane blue $\mu$ LED (450 nm)	251 MHz	660 Mbps	ref. <sup>94</sup>
2021	c-plane blue $\mu$ LED (467 nm)	1.3 GHz	2 Gbps	ref. <sup>95</sup>
2020	Semipolar green $\mu$ LED (525 nm)	775 MHz	1.5 Gbps	ref. <sup>96</sup>

1- $\mu\text{m}$ -thick GaN buffer layer, a 2.5- $\mu\text{m}$ -thick Si-doped n-GaN, an MQW active region, a 30-nm-thick electron barrier layer, and a 75-nm-thick p-GaN contact layer. The sample with a thin QW/QB had a faster recombination process than that of a standard sample with a 3 nm/10 nm InGaN/GaN MQW, which was attributed to the higher EH wavefunction overlap in the thin QW. At 2.5-kA/cm<sup>2</sup> injection current density, the bandwidth of the thin QW/QB device was 536 MHz. Xu et al. designed and fabricated c-plane blue  $\mu\text{LEDs}$  with a thin InGaN layer<sup>90</sup>. Figure 3(a) shows a transmission electron microscopy (TEM) image of the epitaxial structure of the fabricated LED. The GaN barrier and InGaN well were 1 nm and 12 nm thick, respectively. A 3D schematic of the device is presented in Fig. 3(b), and a cross-sectional scanning electron microscopy (SEM) image of the  $\mu\text{LED}$  device is shown in Fig. 3(c). The 60  $\mu\text{m}$  LED pixels were defined using ICP etching processes. Figure 3(d) depicts the modulation bandwidth of the  $\mu\text{LED}$  devices. The bandwidth eventually reaches a high value of 1.53 GHz at 6 kA/cm<sup>2</sup>. Evidently, a 1 nm ultrathin QW structure sig-

nificantly reduces the QCSE, resulting in a high recombination rate.

Dry-etching technology can cause inevitable and significant deterioration of  $\mu\text{LED}$  performance, and consequently cannot meet the requirements to manufacture high-performance  $\mu\text{LEDs}$ <sup>29,99</sup>. In addition, with conventional biasing methods, small changes in the forward bias will result in large fluctuations in the injection current density when the LED is operating at a high injection current density, which is difficult to maintain and control. Cai et al. demonstrated the growth of LEDs on predetermined microhole arrays created by SiO<sub>2</sub> masks on a high-electron-mobility transistor (HEMT) template<sup>100</sup>. In this study, direct modulation of the LED emission was achieved by adjusting the 50-nm HEMT gate voltage. The fabrication method is illustrated in Fig. 3(e–h). First, a SiO<sub>2</sub> layer was deposited on the AlGaIn/GaN template. Subsequently, SiO<sub>2</sub> was etched into the microhole arrays. Then, metalorganic vapor-phase epitaxy (MOVPE) was used to reload the patterned HEMT template for further LED growth. The maximum modulation bandwidth



**Fig. 3** | (a) Transmission electron microscopy (TEM) image. (b) Three-dimensional schematic and (c) scanning electron microscopy (SEM) image of a  $\mu\text{LED}$ . (d)  $-3$  dB bandwidth for different current densities. Schematics of fabrication for the growth of  $\mu\text{LEDs}$  on a high-electron-mobility transistor (HEMT) template. (e) Deposition of SiO<sub>2</sub>. (f) Fabrication of SiO<sub>2</sub> microhole arrays. (g) Growth of  $\mu\text{LEDs}$ . (h) SiO<sub>2</sub> mask removal. (i) Modulation bandwidth and (j) electroluminescence (EL) spectra of device. Figure reproduced with permission from: (a–d) ref.<sup>90</sup>, IEEE; (e–j) ref.<sup>100</sup>, under a Creative Commons Attribution (CC-BY) License.

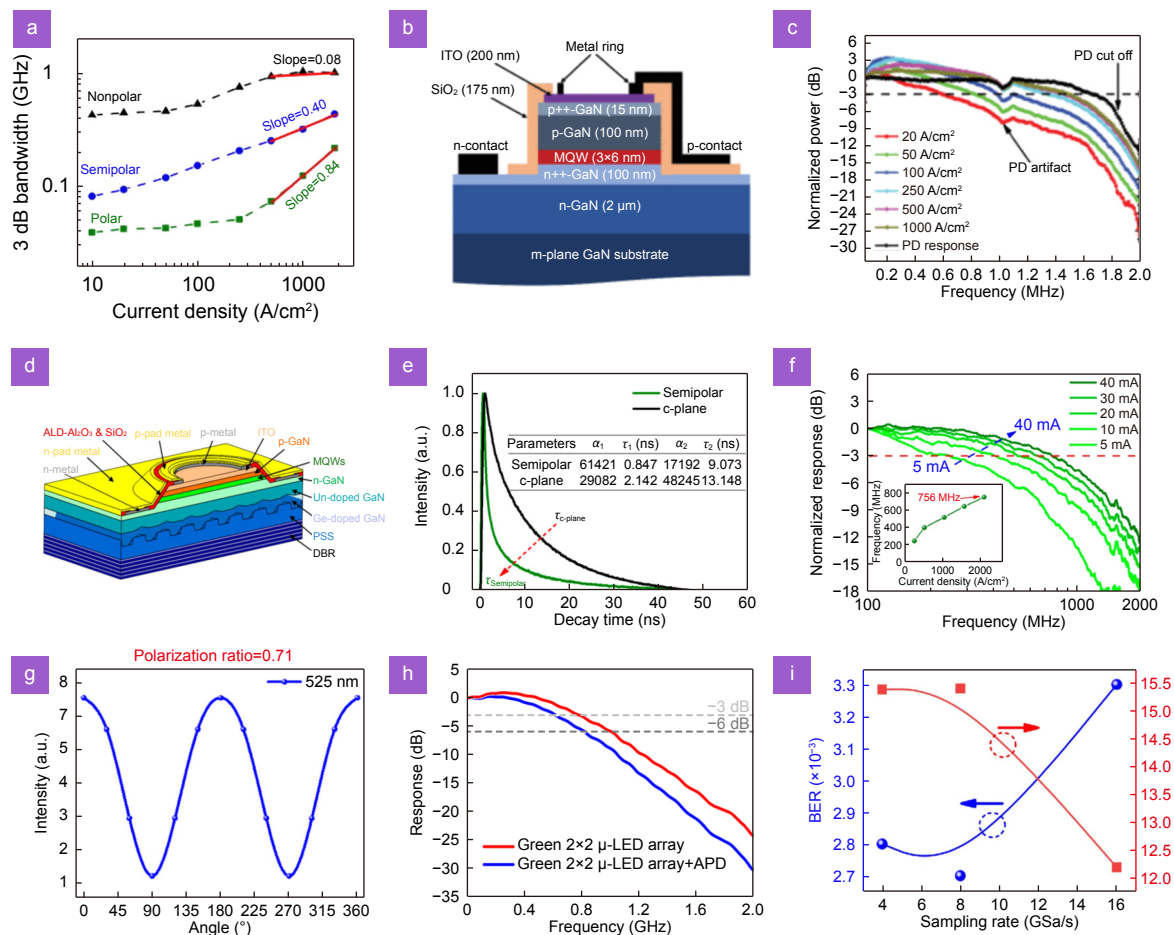
reached 1.2 GHz (Fig. 3(i)), which was realized with a 10 V bias in relation to the HEMT and zero gate bias. Figure 3(j) shows the electroluminescence (EL) spectra of a single  $\mu$ LED.

### Nonpolar and semipolar plane growth

C-plane LEDs are affected by a strong QCSE, which limits the modulation bandwidth and leads to a decrease in efficiency at high injection current densities<sup>66,68</sup>. The deleterious effects of these fields have recently sparked growing interest in nontraditional directions. One approach to overcome the QCSE is to fabricate nonpolar or semipolar structures<sup>101</sup>. Monavarian et al. measured the modulation bandwidths of  $\mu$ LEDs with different crystal orientations, as shown in Fig. 4(a)<sup>65</sup>. The bandwidth of the  $\mu$ LEDs grown on nonpolar faces is the highest, followed by those of the semipolar plane and c-

plane. The difference in the bandwidth is related to the difference in the wavefunction overlap between the different crystal orientations. Corresponding to the modulation bandwidth, the wavefunction overlap is the highest in nonpolar QWs. When the growth direction of the InGaN/GaN MQW crystal planes is perpendicular to the polar plane, such as (11–20) or (1–100), the polarization field can be completely eliminated<sup>102</sup>.

Rashidi et al. demonstrated a nonpolar m-plane blue  $\mu$ LED for high-speed VLC<sup>103</sup>. As depicted in Fig. 4(b), the device is grown on a freestanding GaN substrate formed by metal–organic chemical vapor deposition on a nonpolar (10–10) face. The normalized frequency responses of the nonpolar  $\mu$ LEDs at different current densities are shown in Fig. 4(c). With an injection current density of 1000 A/cm<sup>2</sup>, the maximum –3 dB bandwidth of the LEDs reached a maximum of 1.485 GHz.



**Fig. 4** | (a) Bandwidth for devices with different crystal orientations. (b) Schematic and (c) frequency response of the nonpolar  $\mu$ LED. (d) Schematic diagram of semipolar (20–21) green  $\mu$ LED structures. (e) Time-resolved photoluminescence (TRPL) curves of semipolar  $\mu$ LED and c-plane  $\mu$ LED. (f) Frequency response of the semipolar  $\mu$ LED. (g) PR and (h) frequency responses of  $\mu$ LED array. (i) BER and signal-to-noise ratio at 4.5 Gbit/s transmission rate with different sampling rates. Figure reproduced with permission from: (a) ref.<sup>65</sup>, AIP Publishing; (b, c) ref.<sup>103</sup>, IEEE; (d–f) ref.<sup>96</sup>, American Chemical Society; (g–i) ref.<sup>109</sup>, Optica Publishing Group.



Although devices grown on nonpolar planes can effectively eliminate polarization fields, achieving long-wavelength emissions  $>510$  nm with such nonpolar a-plane or m-plane LEDs remains challenging. Additionally, nonpolar LEDs have a low EQE, owing to low In incorporation. The semipolar plane is also a fundamental solution to the QCSE, which makes semipolar  $\mu$ LEDs a strong contender for high-bandwidth devices. The chemical potential for incorporating In atoms into semipolar planes is considerably lower than that into nonpolar planes, owing to the lower repulsive interactions between the semipolar GaN surface and the In atoms. This facilitates the growth of long-wavelength InGaN/GaN devices<sup>104</sup>. Chen et al. realized 540-nm green  $\mu$ LEDs with a high  $-3$  dB bandwidth using semipolar (20–21) GaN epitaxy<sup>96</sup>. Figure 4(d) demonstrates the optimized  $\mu$ -LED device structure. The Al<sub>2</sub>O<sub>3</sub> layer deposited by atomic-layer deposition (ALD) reduced the effect of sidewall defects. The carrier lifetime  $\tau$  of the semipolar  $\mu$ LED measured by time-resolved photoluminescence (TRPL) is 2.65 ns, as shown in Fig. 4(e), which is much lower than that of the c-plane  $\mu$ LED used as a reference. The shorter lifetime of the semipolar samples is owing to the weak polarization field. This results in a larger electron-hole wavefunction overlap, which reduces  $\tau_r$ <sup>105–107</sup>. A shorter carrier recombination corresponds to faster carrier transport; thus, green semipolar  $\mu$ LEDs can achieve  $-3$  dB bandwidths up to 756 MHz, as shown in Fig. 4(f).

The fast response time and small size of semipolar  $\mu$ LEDs enable a high output power, high modulation bandwidth, and high efficiency when integrated into arrays<sup>108</sup>. Lin et al. designed a 2×2 semipolar green  $\mu$ LED array with a size of 50  $\mu\text{m}$ <sup>109</sup>. Semipolar (20–21) oriented GaN layers were synthesized on a patterned sapphire substrate. All the elements in the  $\mu$ LED array were connected in parallel. The device was fabricated by employing nanostructured grating patterns, which improved the polarization ratio (PR)<sup>110</sup>. Figure 4(g) reveals that the output degree of polarization (DOP) of the semipolar  $\mu$ LED increased by 0.71 to favor liquid-crystal display applications. With an injected current of 23 mA, the  $-3$  dB bandwidth of the  $\mu$ LED array was 800 MHz, as shown in Fig. 4(h). A transmission rate of 4.5 Gbps can be achieved using 8-QAM OFDM modulation, as shown in Fig. 4(i).

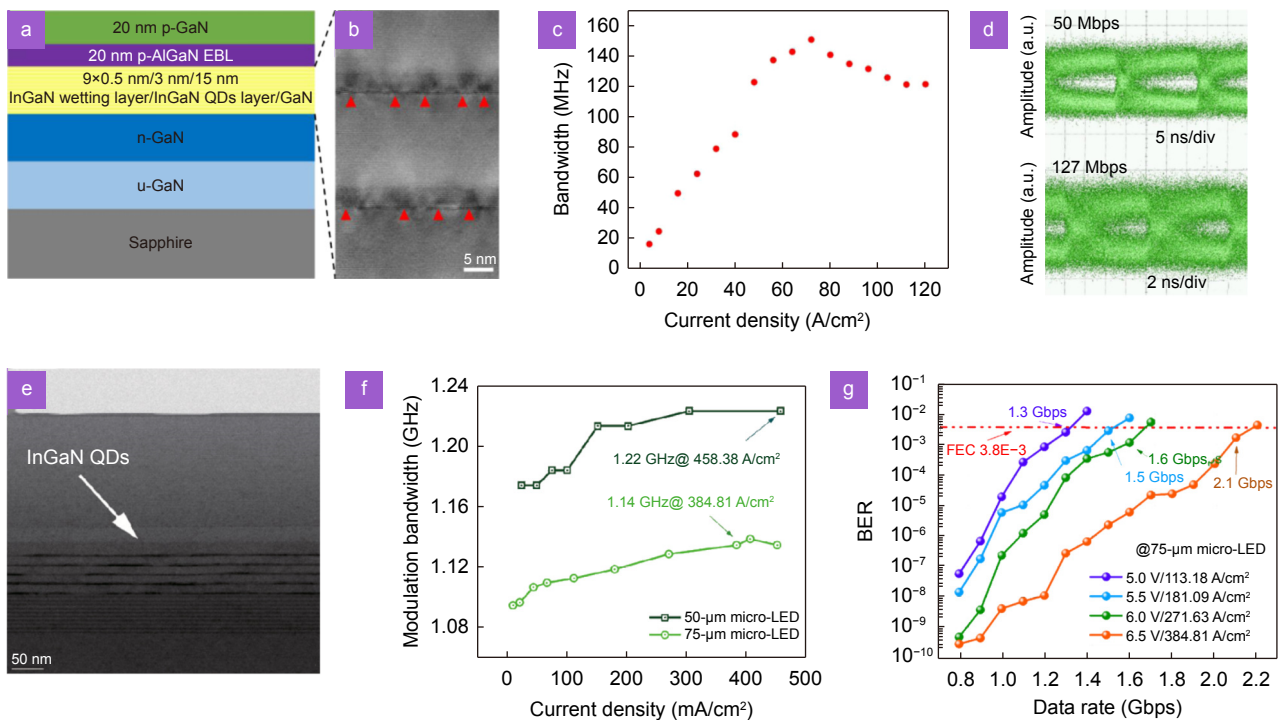
### InGaN QDs in active region

GaN-based QDs have received significant research atten-

tion, owing to their strong quantum-confinement capabilities<sup>111–114</sup>. Unlike QWs, which only bear compressive stress from the direction parallel to the interface, the compressive stresses on QDs in three dimensions cancel each other; thus, the strain is smaller than that of QWs. In addition, QDs exhibit a stress-releasing mechanism during epitaxy<sup>115</sup>. Incidentally, the use of QDs instead of QWs can reduce the volume of the active region, which is beneficial for accelerating the carrier recombination process and increasing the device modulation bandwidth.

Based on the potential of GaN-based QDs devices in VLC applications, Wang et al. grew self-assembled QDs in the Volmer-Weber mode<sup>93</sup>. This resulted in QDs without a wetting layer (WL), owing to a sufficiently large lattice mismatch. The WL in the QD decreases the carrier localization, thereby limiting the recombination and increasing the carrier lifetime<sup>112</sup>. Thus, the bandwidth of the  $\mu$ LED device reaches 1.3 GHz at a relatively low current density of 509 A/cm<sup>2</sup>.

QCSE suppression was also observed in QD-based long-wavelength LEDs, with a blue-shift level similar to those of nonpolar or semipolar plane devices with increasing injection current<sup>116,117</sup>. Wan et al. demonstrated a phosphor-free single-chip WLED using a InGaN QDs structure<sup>118</sup>. Figure 5(a) shows a schematic of the epitaxial structure. A HRTEM image of the MQW region is shown in Fig. 5(b), where alternately stacked light and dark layers represent GaN QBs and InGaN QWs, respectively. The modulation bandwidth of the WLED at different current densities is summarized in Fig. 5(c). The bandwidth of a traditional WLED (a few MHz) is much lower than that of the fabricated WLED. One reasonable explanation is that the QCSE of InGaN/GaN QDs is smaller than that of the InGaN/GaN QWs. The  $-3$  dB bandwidth reached a maximum of 150 MHz. Eye diagrams for transmission rates of 50 and 127 Mbps are shown in Fig. 5(d). Wei et al. designed a green  $\mu$ LED with five-layer InGaN QDs<sup>91</sup>. Figure 5(e) shows a TEM image of the 5-layer InGaN QD structure as the active region. The heights of QDs are distributed over approximately 2–3 nm, and the horizontal distribution is denser, which helps shorten the carrier recombination lifetime. Figure 5(f) shows the extracted  $-3$  dB bandwidth. The bandwidth of QD green  $\mu$ LEDs with 50 and 75  $\mu\text{m}$  active region diameters can reach 1.22 and 1.14 GHz, respectively. As shown in Fig. 5(g), the 75  $\mu\text{m}$  sample can achieve a maximum transmission rate of 2.0 Gbps.



**Fig. 5 |** (a) Schematic. (b) HRTEM image of the QWs. (c) Bandwidth of single chip WLED vs. injection current density. (d) Eye diagram at transmission rate of 50 and 127 Mbps. (e) TEM images of InGaIn QDs. (f)  $-3$  dB bandwidth and (g) BER at different current densities. Figure reproduced with permission from: (a–d) ref.<sup>118</sup>, Optica Publishing Group; (e–g) ref.<sup>91</sup>, ACS Publishing.

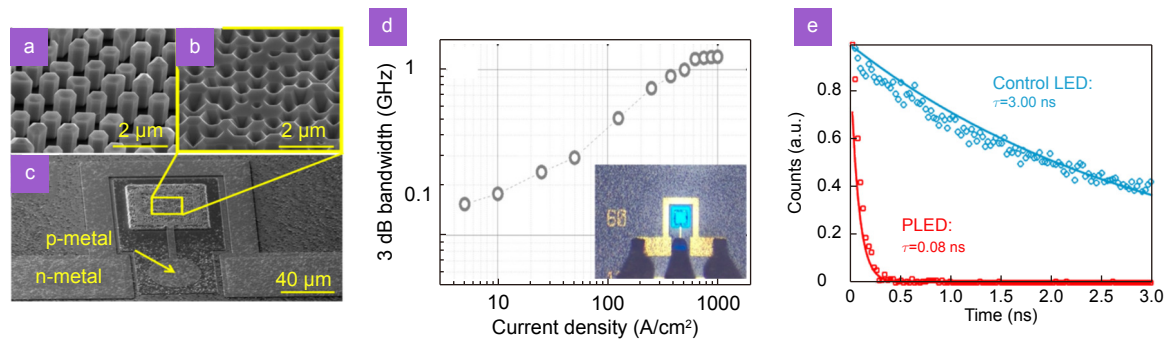
### Microstructure

Exploiting nanostructures in the active region to excite resonant interaction between QWs and QDs in QD-LEDs is another approach to fabricate high-modulation bandwidth devices. Nonradiative resonance energy transfer (NRET) between QWs and QDs has been demonstrated to use exciton-exciton coupling to accelerate the recombination rate<sup>119–121</sup>. Wan et al. fabricated quantum-well-QD-SP coupled LEDs in nanopore LED (H-LED) structures filled with QD and silver nanoparticles, which had a shorter carrier lifetime compared to H-LED and QD-only filled samples (QD-LEDs)<sup>122</sup>. In QD-LEDs, excitons close to the nanohole sidewall can undergo NRET. This process can significantly increase the decay rate of excitons in QWs and lead to shorter carrier lifetimes. Owing to the NRET, the recombination of excitons in the QWs of quantum-well-QD-SP coupled LEDs is faster than that of QD-LEDs, which further decreases the fast carrier lifetimes.

Similar to QDs, InGaIn nanowires are another low-dimensional structure. Unlike planar  $\mu$ LEDs, nanowire  $\mu$ LEDs have independent nanowires within each pixel. Thus, the surface-to-volume ratio remains constant for different pixel sizes<sup>123,124</sup>. This enables a higher efficiency in nanowire  $\mu$ LEDs. Nanowire-based LEDs can also be

considered in VLC applications. Nami et al. grew GaIn nanowires on *c*-plane sapphire substrates using MOCVD<sup>125</sup>. InGaIn/GaIn QW/barriers were grown around the core-shell nanowires and 60  $\mu$ m nanowire  $\mu$ LEDs were fabricated. SEM images of the nanowires after QW and p-GaIn growth and the fully fabricated nanowire  $\mu$ LED device are shown in Fig. 6(a–c), respectively. The nanowires contained nonpolar *m*-plane sidewalls. The bandwidth of the nanowire  $\mu$ LED was 1.19 GHz, as shown in Fig. 6(d). The high modulation bandwidth of nanowire  $\mu$ LEDs is the result of electron-hole wavefunction overlap in nonpolar QWs, which increases the rate of recombination processes.

Recently, plasmonic devices have received extensive attention in the field of VLC for surface plasmons, which can create energy transition channels for electron-hole pairs in devices via QW-SP coupling<sup>122</sup>. Possible resonant coupling conditions between QWs and bulk silver have been reported<sup>126</sup>; therefore, the plasmonic coupling is extensively used in GaIn-based LEDs<sup>127,128</sup>. Ferrari et al. fabricated a nanostructured plasmonic light-emitting diode (PLED)<sup>129</sup>. Nanoholes were patterned into the MQW region through the p-GaIn layer and then coated with a thin Ag film. This scheme exploits the nanostructural properties of silver films to couple SPP to the far field.



**Fig. 6** | SEM images of the nanowires after (a) QW and (b) p-GaN growth and (c) the fully fabricated nanowire  $\mu$ LED device. (d)  $-3$  dB bandwidth of device. (e) TRPL of PLED and control LED. Figure reproduced with permission from: (a–d) ref.<sup>125</sup>, American Chemical Society; (e) ref.<sup>129</sup>, American Chemical Society.

The decay curves of the PLED versus the control LED are shown in Fig. 6(e). The lifetimes of PLED and control LED are 0.08 ns and 3 ns, respectively, which is equivalent to a shortening by a factor of several dozen. This paves the way for the fabrication of high-speed ion-enhanced  $\mu$ LEDs used for VLC.

### $\mu$ LED-based WLED VLC system

VLC technology enables LED-based lighting infrastructure to offer both lighting and data communication. According to statistics, lighting electricity accounts for approximately 20% of the global electricity consumption, which urgently requires the development of efficient and environmentally friendly lighting sources. Therefore, compared with monochromatic blue or green LEDs, WLEDs that can provide lighting functions while offering a high luminous efficiency, long service life, and environmental protection characteristics have greater application prospects in VLC. In recent years, VLC systems utilizing WLEDs have been demonstrated<sup>130–132</sup>.

#### PL WLEDs

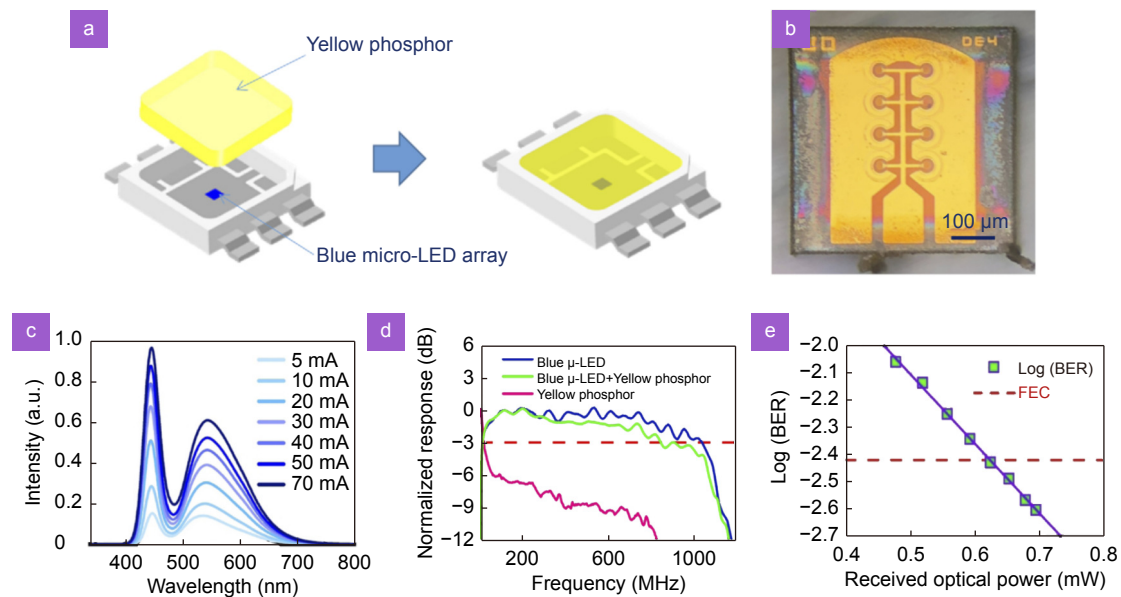
WLEDs based on  $\mu$ LEDs are attractive, owing to the characteristics of a high modulation speed, high efficiency, and long lifetime. The ideal white  $\mu$ LED is a monolithic integration of three separate  $\mu$ LED chips containing red, green, and blue (RGB) emissions. Research on high-efficiency blue  $\mu$ LEDs is relatively mature. However, the “green gap” limits the performance of the green  $\mu$ LED<sup>133</sup>. Green  $\mu$ LEDs have a high proportion of indium, which requires a relatively low temperature when fabricating, which leads to strong QCSEs and a reduced radiative recombination efficiency. In addition, red  $\mu$ LEDs are mainly fabricated using the AlGaInP material system, which leads to long carrier diffusion length

and enhanced non radiation recombination<sup>134,135</sup>. Therefore, the efficiency degradation of red  $\mu$ LEDs is more severe with the size of devices decreasing to a few microns. Another problem with implementing RGB  $\mu$ LEDs is that the working voltage between different pixels is different, which complicates driver circuit design. For photoluminescent WLEDs, trichromatic components are typically derived from emissive materials pumped by blue or UV chips.

#### WLEDs based on phosphor film for VLC

Phosphor-based WLEDs based on blue LEDs exciting yellow phosphor are among the most common lighting devices. However, the modulation bandwidth of WLEDs is significantly limited by the long response time of LEDs and fluorescent materials. This leads to difficulties in realizing high-speed VLC with the electro-optic (EO) bandwidth of conventional WLEDs of only a few MHz. Therefore, previous studies have proposed several methods to increase speed, including the addition of equalization circuits or higher-order modulation methods. Minh et al. increased the bandwidth of a WLED to 50 MHz using an analog equalizer and achieved a transmission rate of 100 Mbps<sup>136</sup>. Hsu et al. proposed the use of adaptive Volterra filtering for phosphor-based WLED VLC systems, and a transmission rate of 700.68 Mbit/s was achieved<sup>137</sup>. Hsu et al. demonstrated a  $3 \times 3$  multiple-input multiple-output (MIMO) WLED VLC system with a data rate of 1 Gbps using a pre-equalizer circuit and OFDM modulation<sup>138</sup>.

To address the low modulation bandwidth of WLEDs fabricated based on phosphor films, blue  $\mu$ LEDs can be integrated with color-conversion materials. Chun et al. achieved high-speed transmission of 1.68 Gbps using a blue  $\mu$ LED combined with phosphor films<sup>139</sup>. Huang et



**Fig. 7 |** (a) Schematic diagram of WLED device based on semipolar  $\mu$ LED array. (b) Photographs of the  $\mu$ LED array without current. (c) Spectrum of the WLED. (d) Measured normalized frequency response of  $\mu$ LED array. (e) BER curve of the white-light VLC system. Figure reproduced with permission from: (a–e) ref.<sup>87</sup>, under the Optica Open Access Publishing Agreement.

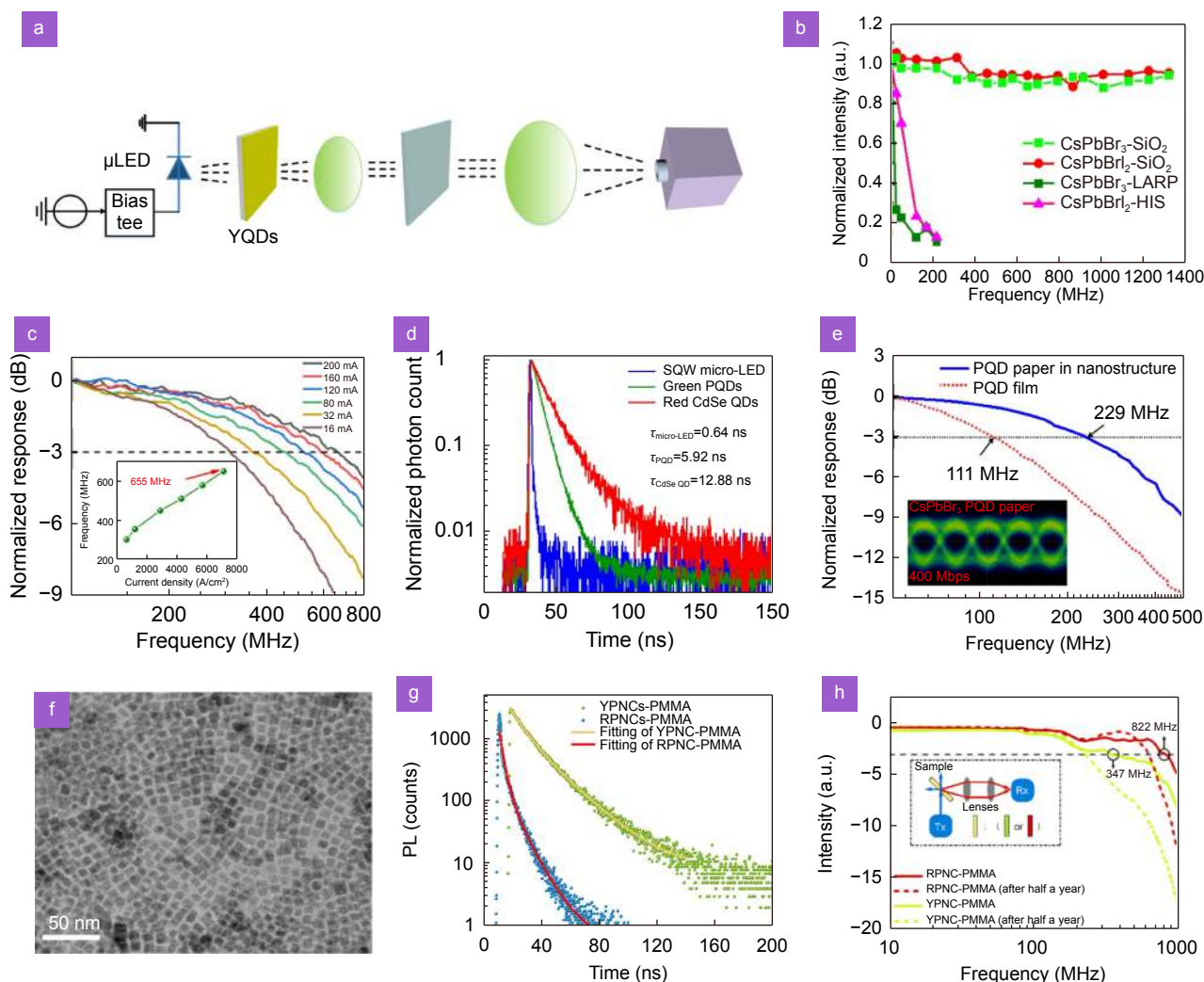
al. proposed a white-light system based on blue  $\mu$ LED arrays with phosphor color conversion to achieve a 127.3 MHz EO bandwidth<sup>140</sup>. Semipolar  $\mu$ LEDs also provide unique advantages in WLED systems, owing to their excellent performance. Zhang et al. utilized semipolar (20–21) blue  $\mu$ LEDs to pump yellow phosphors to realize a high-speed VLC system<sup>87</sup>. A phosphor film was coated onto the surface mounted devices (SMD) package to generate white light, as shown in Fig. 7(a). Figure 7(b) shows a photograph of the fabricated WLED device. The optoelectronic and communication properties of these devices were also evaluated. The spectrum of the blue  $\mu$ LED array with yellow phosphor is displayed in Fig. 7(c), with peak wavelengths of 447 and 545 nm. The normalized frequency response of the  $\mu$ LED array was measured, as shown in Fig. 7(d). The bandwidth of the semipolar blue  $\mu$ LED, yellow component and the overall white-light VLC system are 1042.5, 24, and 849 MHz, respectively. Figure 7(e) shows the BERs curves of the white-light VLC system. A data rate of 2.805 Gbps can be achieved using OFDM modulation; thus, this phosphor-based white  $\mu$ LED device can be applied to high-speed VLC.

#### WLEDs based on QDs color conversion for VLC

Despite the excellent performance of phosphor-based WLEDs, their modulation bandwidth is significantly limited by the color-conversion materials. The radiative relaxation of phosphors is related to the trap energy state

with a certain depth, which causes the afterglow lasting a few microseconds<sup>37,141–143</sup>. Therefore, the development of color-conversion materials with a fast response speed is crucial for VLC applications. QDs are nanoscale semiconductor crystals that can modulate the emission wavelength by changing sizes<sup>144–146</sup>. Compared to traditional fluorophores, QDs have a wide range of absorption spectra, including blue and UV bands<sup>147,148</sup>. More importantly, for VLC applications, QDs typically have short fluorescence lifetimes in the order of nanoseconds. Therefore, QD-based color-conversion layers can achieve high modulation bandwidths and high data rates. Ruan et al. demonstrated that AgInS<sub>2</sub>/ZnS core/shell QDs are good color-conversion materials for WLEDs and can conduct VLC<sup>149</sup>. Xiao et al. increased the modulation bandwidth of QD-WLED by 67.75% using CdSe/ZnS QDs<sup>130</sup>. Cao et al. used GHz high-bandwidth blue LED devices combined with CdSe/ZnS QDs to achieve white light emission with an overall modulation bandwidth of 637.6 MHz for visible light communication<sup>150</sup>.

Halide perovskite quantum dots (PQDs) exhibited narrow emission and short fluorescence lifetimes and have garnered broadening research interest for VLC<sup>151</sup>. Shi et al. combined blue GaN-based  $\mu$ LEDs with CsPbBr<sub>1.8</sub>I<sub>1.2</sub> yellow PQDs for color conversion to fabricate a white-light VLC system, as illustrated in Fig. 8(a)<sup>152</sup>. Modulation bandwidths of 73 MHz and 85 MHz were achieved for PQDs and overall VLC system, respectively.



**Fig. 8** | (a) White-light VLC system consisting of perovskite quantum dot (PQD) and blue  $\mu$ LED. (b) The longevity of the PL properties of the PNCs. (c) Frequency response of the PNC- $\mu$ LED. (d) TRPL measurement for semipolar  $\mu$ LED, PQD and CdSe QD papers. (e) Frequency response of PQD paper and PQD film. (f) TEM images of RQDs. (g) TRPL measurement for YQDs and RQDs. (h) Frequency response of red and yellow PNC-PMMA. Figure reproduced with permission from: (a) ref.<sup>152</sup>, American Chemical Society; (b, c) ref.<sup>139</sup>, American Chemical Society; (d, e) ref.<sup>153</sup>, Optica Publishing Group; (f–h) ref.<sup>154</sup>, American Chemical Society.

Wu et al. proposed a PNC- $\mu$ LED device based on a semi-polar (20–21) blue  $\mu$ LED array, mixing green CsPbBr<sub>3</sub> and red CsPbBr<sub>2</sub> PNCs powders as the color conversion layer<sup>139</sup>. The PNCs were encapsulated in a SiO<sub>2</sub> shell using high-temperature sintering, which significantly improved the stability. Figure 8(b) illustrates the PL intensity of PNCs after blue radiation aging. The SiO<sub>2</sub>-embedded samples exhibited remarkable stability and no degradation under blue irradiation. The bandwidth of PNCs is typically in the order of tens of MHz, and a filter was used to remove the red and green light generated by PNCs in the experiment. The blue light passing through the filter was coupled to a photodetector, and the highest bandwidth of the PNC- $\mu$ LED was measured as 655 MHz at a current of 200 mA (Fig. 8(c)).

Currently, the in-depth study of PQDs is committed to fabricating color-conversion layers with higher modulation speeds, which will further increase the transmission rate. Singh et al. proposed a flexible white-light VLC system consisting of nanostructured green CsPbBr<sub>3</sub> PQD paper, red CdSe QD paper, and semi-polar blue  $\mu$ LEDs<sup>153</sup>. CsPbBr<sub>3</sub> PQD paper was prepared by mixing a QD solution with a cellulose nanocrystal suspension. The PQD paper fabricated using this method has a nanostructure that provides a strong quantum confinement effect to increase the recombination rate. The TRPL measurements of PQD and CdSe QD are shown in Fig. 8(d), and the calculated average lifetimes are calculated as 5.92 and 12.88 ns, respectively. The shorter carrier lifetime of the PQD paper is attributable to the quantum confinement

effect. The PQD paper exhibits a higher bandwidth of 229 MHz compared to the 111 MHz of the PQD film embedded in the polymer fabrication, as shown in Fig. 8(e), which is suitable for achieving a high-speed VLC. Wang et al. proposed a white-light VLC system using red/yellow-emitting CsPb(Br/I)<sub>3</sub> and CsPbI<sub>3</sub> PNC-PMMA films combined with blue  $\mu$ LEDs<sup>154</sup>. Figure 8(f) shows the TEM images of RQDs with an average size of  $5.73 \pm 0.95$  nm. The carrier lifetimes of yellow PNC-PMMA and red PNC-PMMA are 11.2 and 3.5 ns, respectively, as shown in Fig. 8(g). Such short lifetimes indicate a higher modulation bandwidth. This was primarily attributed to the small average size of the red QDs, which led to significantly accelerated carrier relaxation rates. The normalized frequency response of the PNC film was further tested (Fig. 8(h)). The -3 dB bandwidths of red and yellow PNC-PMMA were 822 and 347 MHz, respectively, which exhibited good potential for indoor high-speed white-light communication systems.

Notably, PQDs contain toxic elements, such as Pb and Cd, which cause pollution and limit the wide application of QDs. The fabrication of QDs without toxic elements has become a subject of intense interest recently. Soheyli et al. reported a novel aqueous-phase approach for the preparation of multicomponent In-based QDs<sup>155</sup>. The absorption and photoluminescence emission spectra of the as-prepared QDs were optimized by altering their composition to obtain Zn-Ag-In-S/ZnS and Cu-Ag-In-S/ZnS QDs. In addition to displays, such QDs are equally promising for VLC applications.

### Electroluminescent WLEDs

Although WLEDs based on color-conversion layers have made significant progress and possess a relatively high luminous efficiency, we emphasize that such a WLED involves energy loss during the down-conversion process. The current efficiency (defined as the ratio of luminance to current) of color-conversion-based WLEDs is lower than that of electroluminescent multicolor QW WLEDs. Therefore, electroluminescent WLEDs without color-conversion layers or phosphors are attractive because they can overcome the drawbacks of phosphor-converted WLEDs, such as Stokes energy conversion loss, and they have good stability<sup>156,157</sup>.

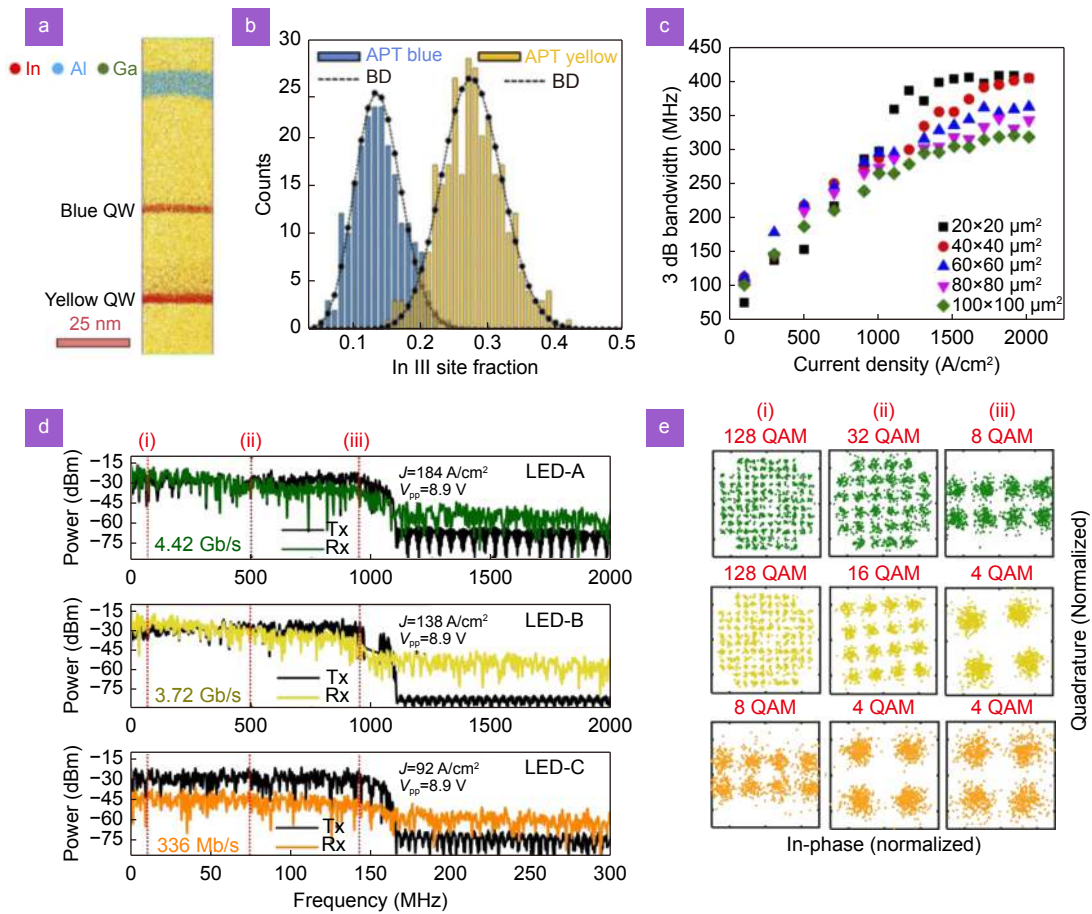
Blue and yellow QWs are typically grown on GaN substrates to produce monolithic WLED devices. During fabrication, the device structure is optimized to realize WLED devices more suitable for VLC. Semipolar GaN

materials have high polarization ratios, a large wavefunction overlap, and short carrier lifetimes, which make monolithic white semipolar GaN  $\mu$ LEDs more attractive. Khoury et al. grew high-efficiency monolithic white semipolar (20–21) LEDs on 4-inch sapphire templates<sup>158</sup>. An overall PR of 0.3 was achieved based on the blue and yellow QWs. The  $\mu$ LEDs in their work achieved high modulation bandwidths of up to 660 MHz. They also reported that the PR increased in devices with longer wavelengths at higher compositions, which suggests that monolithic white semipolar LEDs have potential applications as LCD backlights<sup>159,160</sup>.

In another study, Li et al. fabricated white semipolar (20–21)  $\mu$ LEDs by adopting a top blue QW and bottom yellow QW directly grown on a (20–21) semipolar bulk GaN substrate<sup>161</sup>. The QWs comprised a 3 nm In<sub>0.28</sub>Ga<sub>0.72</sub>N yellow QW and a 3 nm In<sub>0.13</sub>Ga<sub>0.87</sub>N blue QW. Figure 9(a) shows the reconstruction side view of the blue and yellow QW and EBL layers. Blue and yellow QWs with different In compositions are clearly observed. Figure 9(b) illustrates the distribution analysis of the In components in blue and yellow QWs. Subsequently, the communication performance of the  $\mu$ LED device was tested. Figure 9(c) indicates the modulation bandwidth for semipolar white  $\mu$ LEDs of all sizes. Devices with sizes of 20 and 40  $\mu$ m achieved high modulation bandwidths of up to 410 MHz. Hagggar et al. fabricated green, yellow, and amber semipolar LEDs on semipolar (11–22) GaN on m-plane sapphire substrates<sup>162</sup>. InGaN SQWs with different In components were used to achieve long-wavelength emissions of different colors. Because all the samples were fabricated using the same material system, a white-light monolithic LED chip can be integrated. The performance of the samples as VLC transmitters was measured. Figure 9(d) shows the received power spectrum of the adaptively loaded OFDM waveform, with maximum data rates of 4.42 Gbps, 3.72 Gbps, and 336 Mbps for the green, yellow, and amber devices, respectively. Figure 9(e) shows the corresponding constellation diagram.

### VLC based on $\mu$ LED detector

As discussed in the previous section,  $\mu$ LEDs with unique properties have been widely used as the transmitter in VLC. However, relatively few studies have used  $\mu$ LEDs as light receivers. Owing to their sensitivity to light, LEDs can potentially be used as PDs. Most commercial PDs are based on Si or GaAs, and the receiving spectrum covers a

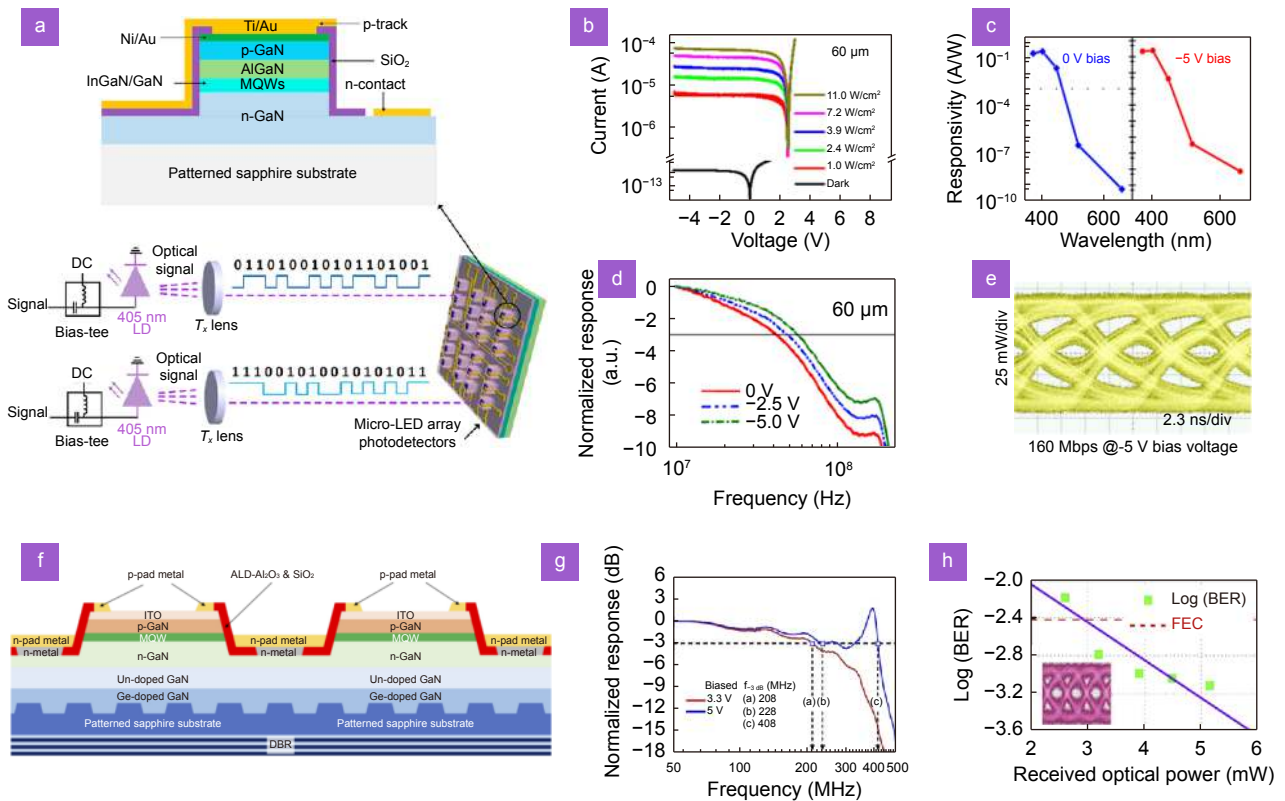


**Fig. 9** | (a) Composition of WLED active region. (b) The distribution analysis of In components in QWs. (c) Modulation bandwidths of different sizes  $\mu$ LEDs. (d) Power spectra of OFDM-modulated waveforms measured at data rates of 4.42 Gbps, 3.72 Gbps, and 336 Mbps. (e) Constellations under corresponding order QAM modulation. Figure reproduced with permission from: (a–c) ref.<sup>161</sup>, under the OSA Open Access Publishing Agreement; (d, e) ref.<sup>162</sup>, under a Creative Commons Attribution (CC-BY) License.

wide range, which causes significant optical noise. In addition to the advantages of low dark current and high sensitivity, GaN-based LEDs offer wavelength selectivity when used as PDs and can only receive light waves lower than their own wavelengths; that is, they have natural filtering properties<sup>43,163,164</sup>. This topic has attracted significant academic interest. There is no need to change the MQW structure or the material of the  $\mu$ LEDs used as PDs. Based on the photoelectric effect, photogenerated electron–hole pairs can realize optoelectronic (OE) conversion when the MQW is excited by the input optical signal. Although the responsivities of  $\mu$ LED-based detectors are generally lower than those of Si or GaAs receivers, they are comparable. Owing to the wavelength selectivity of LED detectors, a higher sensitivity can be achieved for a certain band than current commercial Si or GaAs receivers<sup>165</sup>. In addition to the advantages of LED-based PDs,  $\mu$ LED-based PDs show great potential for realizing high-speed MIMO VLC for light detection.

Owing to the small size and easy integration of  $\mu$ LEDs,  $\mu$ LEDs array-based PDs can enable multi-user communication and increased data rates, compared with individual  $\mu$ PDs. Thus,  $\mu$ LED displays can be used as both transmitters and detectors to achieve duplex high-speed VLC.

As part of the  $\mu$ LED array for VLC detectors, Liu et al. proposed a blue  $\mu$ LED array for use as a PD in VLC<sup>165</sup>. That study realized a  $\mu$ LED PD-based  $2 \times 2$  MIMO VLC (Fig. 10(a)). Two LDs were used as transmitters, and a  $\mu$ LED array was used as the detector. Figure 10(b) illustrates the I–V characteristics of the  $\mu$ LED PD measured in the dark and under illumination. As observed in the figure, the current of the  $\mu$ LED PD gradually increases with the increase in the received power, owing to the photogenerated carriers. Additionally, for  $\mu$ LED-based PDs, at zero bias, high photosensitivity was observed owing to the low dark current. Figure 10(c) shows the measured responsivity of the  $\mu$ LED PD for different



**Fig. 10 |** (a) Cross-section of the  $\mu$ LED and schematic setup for VLC system using the  $\mu$ LED based photodetectors. (b) Current–voltage (I–V) curves of the  $\mu$ LED-based PD with diameters of 60  $\mu$ m under darkness and illumination. (c) Responsivities of the  $\mu$ LED-based PD measured for various laser wavelengths. (d) Frequency response for  $\mu$ LED-based PD. (e) Eye diagrams at a transmission rate of 160 Mbps. (f) Cross-section of semipolar green  $\mu$ LEDs. (g) Frequency responses of  $\mu$ LED PD. (h) BERs with  $\mu$ LEDs as PD at a transmission rate of 540 Mbps. Figure reproduced with permission from: (a–e) ref.<sup>165</sup>, American Chemical Society; (f–h) ref.<sup>166</sup>, under the OSA Open Access Publishing Agreement.

wavelength bands. The figure reveals that the  $\mu$ LED PD does not respond to wavelength bands above 450 nm, reflecting outstanding wavelength selectivity. The frequency response characteristics of  $\mu$ LED PDs under 405-nm LD illumination are illustrated in Fig. 10(d). Bandwidths up to 41.2 MHz can still be achieved at 0-V bias. Figure 10(e) shows an eye diagram captured by the  $\mu$ LED PD at a transmission rate of 160 Mbps and a bias of -5 V. The obtained results demonstrate the ability of  $\mu$ LED PDs to detect fast optical signals for high-speed communications.

In the previous discussion, we stated that semipolar  $\mu$ LEDs had a high application potential as VLC transmitters, owing to their higher response speed. However, semipolar  $\mu$ LEDs can also achieve high-speed signal detection, owing to their shortened carrier lifetime. Chang et al. investigated the performance of green semipolar (20–21)  $\mu$ LEDs as VLC photoreceivers<sup>166</sup>. The cross-section of the semipolar  $\mu$ LED array used as a PD with a diameter of 30  $\mu$ m is illustrated in Fig. 10(f). Devices grown in the semipolar direction can provide higher

modulation responses, owing to the larger overlap of electron-hole wave functions and shortened carrier lifetime. A VLC system was built with the semipolar  $\mu$ LED as the receiver. The OE responses of the semipolar  $\mu$ LED PD were measured under different biases, as shown in Fig. 10(g). At a bias of 5 V, the measured 3 dB OE bandwidths are 228 MHz, which are considerably larger than those of the LED PDs and other  $\mu$ LED PDs. Figure 10(h) shows the experimental BER curves obtained using the  $\mu$ LED PD array at a data rate of 540 Mbps. This indicates that semipolar  $\mu$ LEDs have a high application value as PDs in high-speed VLC systems.

## Novel applications of VLC towards 6G

The development of next-generation cellular networks has aimed at faster and more reliable solutions with expansive and more complex feature sets. Networks for 6G will have higher transmission speed requirements<sup>167,168</sup>. Studies on epitaxial design, crystal orientation, and microstructure have enabled the fabrication of  $\mu$ LEDs with high-speed modulation characteristics that have



demonstrated Gbps-level data throughput. This will promote the development of  $\mu$ LED-based VLC systems as a key wireless technology for 6G. In addition, the use of high-frequency waves raises user concerns about the potential hazards of radio frequencies to humans in these frequency bands. From this perspective, the VLC system will provide users with the option of using an RF-free connection<sup>169</sup>. Adding this optical-transport interface gives device manufacturers a competitive advantage. Therefore, optical wireless communications must create a viable concept that complements RF communications as part of 6G.

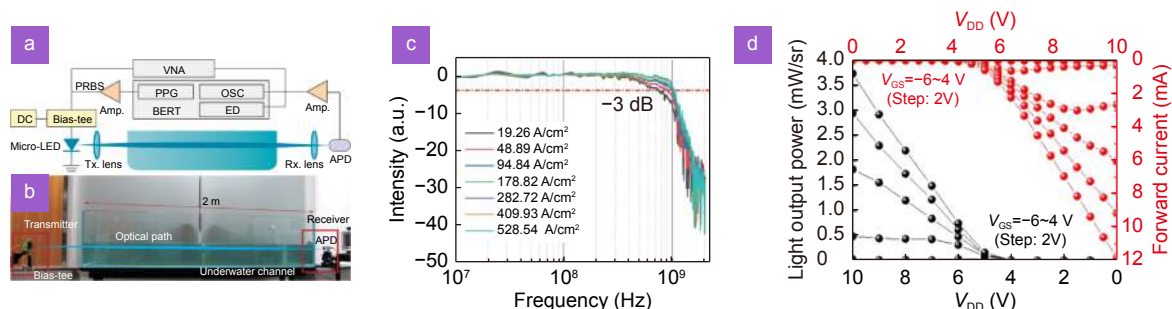
### Underwater VLC technology

Global extensive access is an important aspect in the development of 6G. However, underwater communication, such as in the oceans, performance has always been unsatisfactory. Underwater communication technology is important for realizing the integration of a 6G network. The realization of functions, such as wireless fusion networking and noncontact interaction, between different devices in the oceans requires underwater communication support.

Acoustic waves are the most used method of underwater communication; however, they have a low carrier frequency, which leads to a limited bandwidth<sup>170</sup>. Although RF waves have a higher transmission bandwidth than sound waves, owing to the skin effect, the transmission distance is directly limited, making it difficult to implement the main task of 6G underwater communication<sup>171,172</sup>. Wavelengths between 450 and 550 nm have considerably less attenuation than other light bands, which indicates that blue–green light is of great significance in underwater communication and lays the foundation for underwater visible-light communication (UVLC). Compared with other wireless communication methods,

UVLC has the advantages of high transmission rate, strong anti-interference ability, and high security<sup>173</sup>.  $\mu$ LEDs have exhibited great potential for medium/short-distance high-speed underwater transmission through a high modulation bandwidth<sup>174</sup>.

Recently, Wei et al. fabricated a QD blue  $\mu$ LED with a size of 75  $\mu\text{m}$  for UVLC<sup>175</sup>. The growth-interruption method was employed to fabricate QD active region. **Figure 11(a)** and **11(b)** illustrate a schematic and a photograph of the experimental setup of the  $\mu$ LED-based UVLC system, respectively, over a 3 m communication distance. At a current density of 582.54 A/cm<sup>2</sup>, the modulation bandwidth of the UVLC system increased to 1.03 GHz (**Fig. 11(c)**). Thus, a transmission rate of 2 Gbps could be achieved with a BER of  $2.03 \times 10^{-3}$ . Kim et al. proposed a  $32 \times 32$  high-power MQW flip-chip blue  $\mu$ LED array ( $\mu$ LED-on-HEMT) integrated into AlGaIn/GaN-based HFETs for UVLC<sup>176</sup>. The uniform optoelectronic properties were obtained for each pixel of the integrated  $\mu$ LED-on-HEMT array. The light output power (LOP) and current of the  $\mu$ LED-on-HEMT device were measured as functions of  $V_{\text{DD}}$  (**Fig. 11(d)**). The LOP was 3.7 mW, and  $V_{\text{DD}}$  was 10 V. Each pixel of the integrated array of  $\mu$ LEDs exhibited a high LOP of modulation at 450 nm, which demonstrated the potential for use in UVLC. Lin et al. also demonstrated that, in addition to serving as transmitters,  $\mu$ LEDs could realize optical detection and underwater charging in duplex UVLC<sup>94</sup>. At 0 V bias, the maximum transmission rate of the  $\mu$ LED PD-based UVLC system was 52.5 Mbps. Under a high received optical power, the device could efficiently collect photogenerated carriers. Through circuit design, the  $\mu$ LED can simultaneously collect DC energy that is irrelevant to the transmission information for charging, while realizing high-speed AC signal detection, which is sufficient to drive a 660 nm LD.



**Fig. 11** | (a) Schematic of setup and (b) photograph and (c) frequency responses of the  $\mu$ LED-based UOWC system. (d) Light output power (LOP) and forward current characteristics of the  $\mu$ LED-on-HEMT arrays. Figure reproduced with permission from: (a–c) ref.<sup>175</sup>, under a Creative Commons Attribution license; (d) ref.<sup>176</sup>, under a Creative Commons Attribution License.

## Visible light communication based on AI discipline

VLC applied to 6G must span multiple scenarios, which will lead to complex and changeable channels. Therefore, signals will be affected by nonlinear distortions during transmission. In addition to the complexity of the channel, the nonlinear response of the transmitter LED and PD may also complicate the model of the VLC system, making fitting it with traditional equalization algorithms difficult.

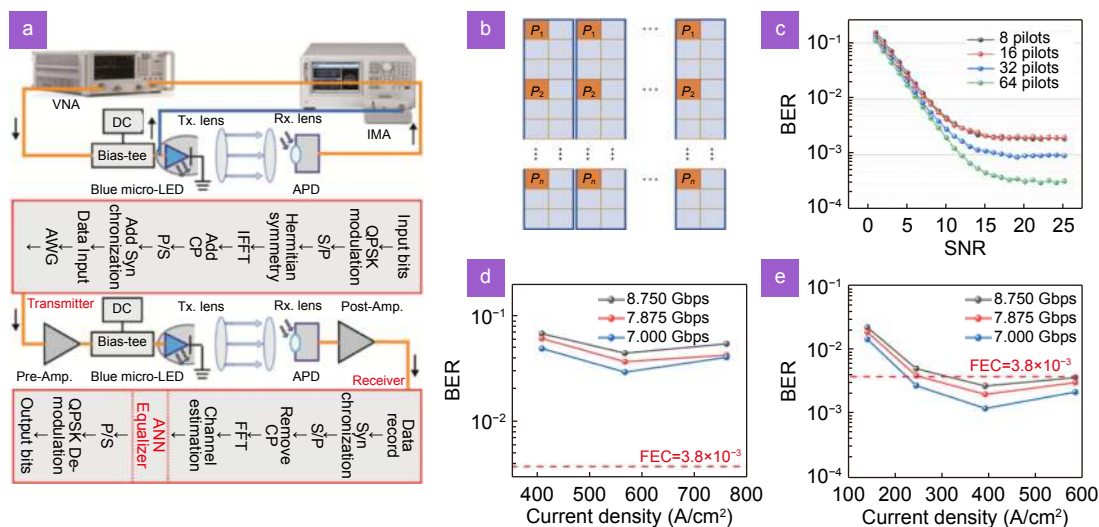
Recently, AI has been widely used in VLC for tasks such as higher-order modulation and demodulation, channel estimation, indoor positioning, and nonlinear equalization. Nonlinearities in high-speed VLC systems can be mitigated by employing clustering schemes and neural networks (NNs). For the application of the clustering, Lu et al. proposed the use of the K-means algorithm to cluster constellation points with a center shift under nonlinear conditions to obtain a new distribution center of constellation points under the condition of deformation<sup>177</sup>. Wen et al. proposed a novel sampling frequency offset mitigation scheme<sup>178</sup>. The algorithm was based on K-means clustering, which enabled the accurate clustering of constellation points with phase offsets. Simultaneously, with the development of GPUs and advancements in digital signal-processing technology, equalizers based on deep NNs (DNNs) are becoming popular. Chi et al. proposed a high-speed kernel-function-based DNN for nonlinear mitigation<sup>179</sup>. Additionally, Chen et al. proposed a hybrid frequency-domain-assisted temporal convolutional NN to compensate for the

nonlinear distortions in UVLC systems<sup>180</sup>.

To meet the requirements of ever-increasing data in the 6G era, various efforts must be made to increase the data rate to the order of 10 Gbps. From a device perspective, combining an NN-based equalizer with  $\mu$ LEDs with a high EO bandwidth is a feasible solution to maximize the transmitted data. In addition to DNNs, the potential of an artificial NN (ANN) program for high-speed communication owing to its approximation to arbitrary functions was demonstrated<sup>181–183</sup>. Wei et al. combined high-bandwidth  $\mu$ LED and ANN equalizers in a VLC system to achieve higher data rates. The ANN consists of five layers<sup>184</sup>. The training dataset was obtained from the Winner channel model dataset. The system structure is illustrated in Fig. 12(a), and a schematic of the arrangement of pilots in the OFDM symbols is shown in Fig. 12(b). The BER simulation results using blocks with pilot lengths of 8, 16, 32, and 64 were measured, as shown in Fig. 12(c). The ANN equalizer achieved relatively good results in the low signal-to-noise (SNR) range. For a specific number of pilots, the BER decreased rapidly and then settled into a higher SNR range. Based on this system, the data rate vs. BER, with two  $\mu$ LEDs as transmitters, was tested (Fig. 12(d) and 12(e)). The 75  $\mu$ m  $\mu$ LED exhibited better performance and could transmit data at a rate of 8.75 Gbps.

## Conclusions

As the research on  $\mu$ LED devices expands, the  $\mu$ LED-based high-speed VLC is garnering increasing interest.



**Fig. 12** | (a) Schematic of the VLC system based on  $\mu$ LED and ANN equalizers. (b) Schematic of the arrangement of pilots. (c) BER in simulation with different pilot lengths. BER performance for (d) 50- and (e) 75- $\mu$ m blue  $\mu$ LEDs. Figure reproduced with permission from ref.<sup>184</sup>, Optical Society of America.

This review summarizes the advantages and challenges of  $\mu$ LEDs in VLC systems. Methods to improve the modulation bandwidth of  $\mu$ LEDs were introduced. In addition to conventional c-polar epitaxial structure optimization and semi/nonpolar GaN epitaxial growth,  $\mu$ LEDs using microstructures or InGaN QDs as active regions can also improve the radiative recombination rate.  $\mu$ LEDs are considered bright solid-state lighting sources compared with different classes of WLEDs for VLC. Similarly,  $\mu$ LEDs can also be used as detectors in VLC systems. Finally, the prospects of VLC in 6G and the latest high-speed VLC applications were introduced. Given the high-speed transmission advantages,  $\mu$ LED-based VLC is expected to become an ancillary technology for 6G and cooperate with other communication technology to benefit our daily lives.

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## Competing interests

The authors declare no competing financial interests.